

LOCAL TIE INFORMATION REPORT

YEBES OBSERVATORY, GUADALAJARA, SPAIN



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1. INTRODUCTION

ITRF is the result of a combination of the different terrestrial reference frames provided by the four space geodetic techniques: GNSS, VLBI, SLR and DORIS. To perform this combination between independent reference frames, it is necessary to have some co-location sites where the various techniques are observing and for which ties have been surveyed in three dimensions.

In Yebes Observatory are co-located four space geodetic technique: two Global Navigation Satellite System (GNSS) antennas and two Very Long Baseline Interferometry (VLBI) radio telescopes, property all of them from the National Geographic Institute (IGN).

The local ties survey accuracy as stated by GGOS should reach 1 mm. In order to get this accuracy, this site has been equipped with a network of geodetic pillars distributed overall the site.

2. ACKNOWLEDGEMENTS

We would like to express our thanks to Geodesy IGN team in Madrid, with special thank to Marcelino Valdés Pérez de Vargas and Jose Antonio Sánchez Sobrino for the working on GNSS calculation as well as the control radiotelescope team of Yebes Observatory who have allowed to us to carry out the tasks related with the radiotelescopes.

We would like also to thank the advices received from BKG (Bundesamt für Kartographie und Geodäsie) and Leica Geosystems.

3. CO-LOCATED SITE DESCRIPTION

3.1. SITE DESCRIPTION

Yebes Observatory is located 70 kilometers far from Madrid, in the center of the Iberian Peninsula, a strategic place in the limit of the European Tectonic Plate.

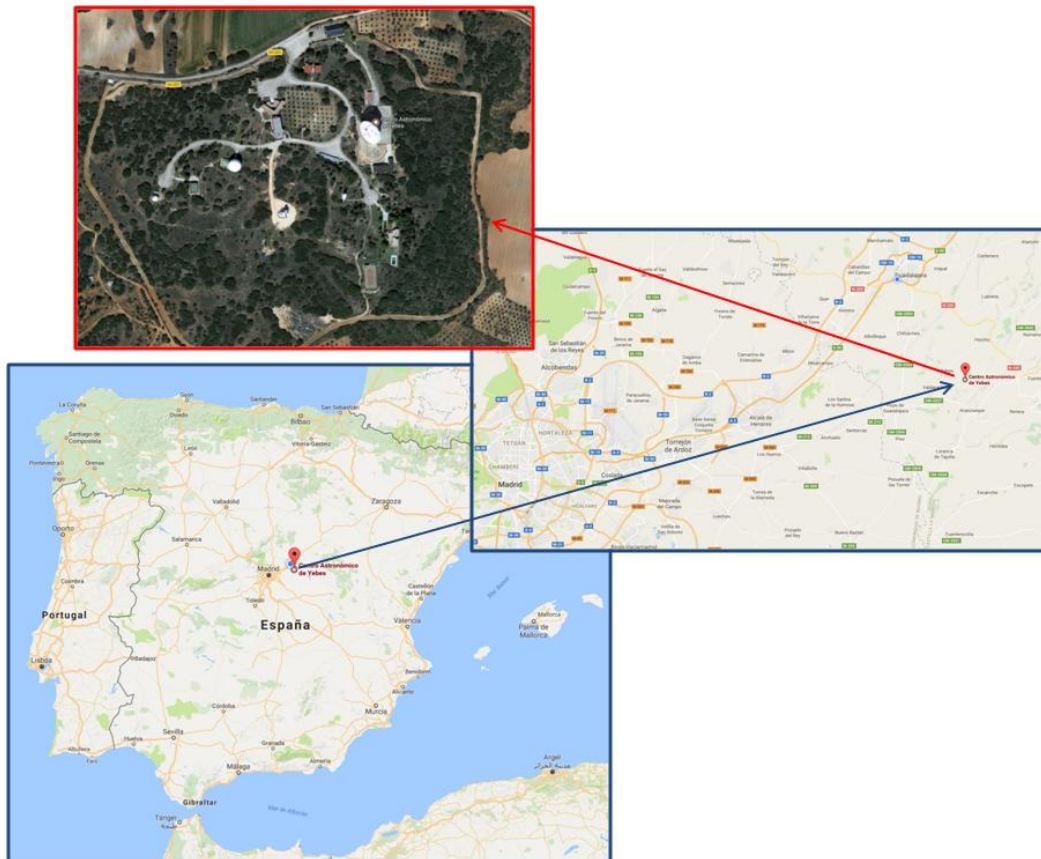


Figure 3.1

3.2. CO-LOCATED POINTS DESCRIPTION

Yebes Observatory is provided with two VLBI antennas (a 40 meter radio telescope and a 13 meters radio telescope), two GNSS antennas (YEBE, on the roof of the office building and YEB1, on the roof of the gravimeter building) and a Superconducting Gravimeter (SG) inside the gravity building. There is also some complementary instrumentation which can be useful as for example a LAMBRECHT rain gauge, a SENTEK ENVIROMENT humidity sensor with 5 depths and a UNIK piezometric sensor to measure the groundwater level. In Figure 3.2 the distribution around the Observatory of the different techniques can be observed and in Table 3.1 a summary with the information of all the spatial techniques is given.



Figure 3.2

Space Geodetic Technique	Name	DOMES number	Antenna type/Receptor type/Support	Code/4-CID
VLBI	YEBES40M	13420S002	40 m. RT. Cassegrain-Nasmith.	7389
VLBI	RAEGYEB	13420S003	13 m. RT. VGOS. RAEGE.	7386
GNSS	YEBE	13420M001	TRM29659.00/ TRIMBLE NETRS/1.2 m. concrete pillar	YEBE
GNSS	YE1	13420M002	LEIAR25/ LEICA GRX+GNSS/1.2 m. concrete pillar	YE1

Table 3.1





3.2.1. GNSS Stations

3.2.1.1. YEBE

YEBE GNSS station was installed in November of 1992 and it is placed on the office building roof. The antenna is set up on a 1.20 meter concrete pillar. The reference point is on the top of the self centering support coincident with the Antenna Reference Point (ARP). See Annex 1.

It belongs to several networks:





- National GNSS Permanent Network (ERGNSS).
- EUREF Permanent Network (EPN).
- International GNSS Service (IGS).
- TEIDE network.

YEBE		DOME: 13420M001	
			
Figure 3.3		Figure 3.4	
General views			
			
Figure 3.5		Figure 3.6	
Invariant reference point			

3.2.1.2. YEB1

YEB1 GNSS station was installed in April of 2009 and it is placed on the office building roof. The antenna is set up on a 1.20 meter concrete pillar.

It belongs to the National GNSS Permanent Network (ERGNSS). The invariant reference point has 6 cm height over the top of the pillar. See Annex 2.

YEB1		DOME: 13420M001	
			
Figure 3.7		Figure 3.8	
General views			
			
Figure 3.9		Figure 3.10	
Detailed antenna view		Invariant reference point	

3.2.2. VLBI Stations

3.2.2.1. YEBES40M- radio telescope

The YEBES40M radio telescope, also called, ARIES XXI, was finished in 2008 and it has a diameter of 40 meters with an alt-azimuth mount. It is dedicated to millimeter and centimeter-wave VLBI and single dish observations. It has receiver to work in S-band (2.2 – 2.37 GHz), CH-band (3.22 – 3.39 GHz), C-band (which is split in two sub-bands, 4.56 – 5.06 GHz and 5.9 – 6.9 GHz), X-band (8.15 -9GHz), K-band (21.77 – 24.45 GHz), and W-band (85-110 GHz). A new Q-band (40-49 GHz) receiver is also in operation.

The VLBI measurements refer to a point in the radio telescope where the elevation axed are projected in to the azimuth axis due to the eccentricity in this radio telescope is near 2 meters. This Invariant Reference Point (IRP) can't be materialized.



Figure 3.11

3.2.2.2. RAEGYEB- radio telescope

The RAEGYEB radio telescope, also called Jorge Juan, has 13.2 meter of diameter with an alt-azimuth mount. It is equipped with a new broadband receiver and it has participated in the first intercontinental VGOS observation in June 2016.

The VLBI measurements refer to a point in the radio telescope where the two rotation axes intersect (azimuth and the elevation axis). This point, IRP, can't be materialized.

This radio telescope has a central pillar, from which measurement to calculate the IRP can be taken.



Figure 3.12

4. LOCAL TIE SURVEY DESCRIPTION

4.1. ORGANIZATION

The local ties survey of Yebes co-location site has been carried out by Javier Lopez Ramasco and Beatriz Córdoba Hita with the cooperation of the IGN (Instituto Geográfico Nacional) geodesy team: Marcelino Valdés Pérez De Vargas, <mvaldes@fomento.es>; José Antonio Sánchez Sobrino, <jassobrino@fomento.es> and Víctor Martín Guijarro <becario.vmg@externomf.es>.

4.2. INSTRUMENT CHARACTERISTICS

All the topometric survey instruments and equipments belong to IGN. Some of them have been brought for the purpose of the survey. Between this instrumentation it can be found:

- A total station Leica TS50 with an accuracy of 0.5" and 0.6mm + 1 ppm in angular and distance respectively. (Figure 4.1)



Figure 4.1

- A Toshiba Satellite Pro NB10T laptop with Bluetooth connection to control the total station. (Figure 4.2)



Figure 4.2

- 8 GPH1P high accurate prisms with an accuracy center of 0.3 mm and 3.500 m reach. (Figure 4.3)



Figure 4.3

- 9 GDF321 tribachs without optical plummet. (Figure 4.4)



Figure 4.4

- 1 GST20-9 wooden tripod. (Figure 4.5)



Figure 4.5

- 8 GRT144 Carrier with 1mm central accuracy. (Figure 4.6)



Figure 4.6

- 5/8" Stub fitting.

- 2 (RRR) Reflector Red-Ring (1.5" diameter). (Figure 4.7)



Figure 4.7

- 1 extra GNSS (Leica GR25 with double frequency and antenna AR20). (Figure 4.8)



Figure 4.8

4.3. SURVEY MONUMENTS

In order to provide the highest accuracy in the determination of the 3D vectors between the different techniques a network of 20 concrete pillars has been built adding the four spatial techniques. In total, 24 survey points have been taken into account. Each geodetic technique is surrounded by pillars that are in the line of sight and so that there is a connection between all the techniques.

The design and construction of the network was not very easy because of the vegetation, trees and low bushes, in the Observatory. It was tried to create baselines with approximately the same length and triangles the most equilateral possible.

To verify the possibility to reach the necessary accuracy for our goal several simulations before the construction the pillars were done.

After the design of the network, pillars were built. They are made of concrete and iron and they are a 30 cm diameter and 1.30 m height cylinder covered by a protecting tube. Between the cylinder pillar and the protecting tube there is a free space of 5 cm to isolate the interior pillar. At the top of the exterior protecting tube, it has a metal lid to prevent the entry of water, and a drainage hole at the bottom of pillar. Fixed to the top of the interior pillar, there is a stainless steel plate of 5 mm thickness, in which center there is a 5/8" standard screw for fixing total station or prism reflector tribrach. (Figures 4.9, 4.10, 4.11).

The construction was done between November 2014 and January 2015.



Figure 4.9



Figure 4.10



Figure 4.11

4.4. OBSERVATION POLYGON

In Figure 4.12 is shown a map of the network with all the visuals between the pillars and in Table 4.1 a list with the information of each pillar.

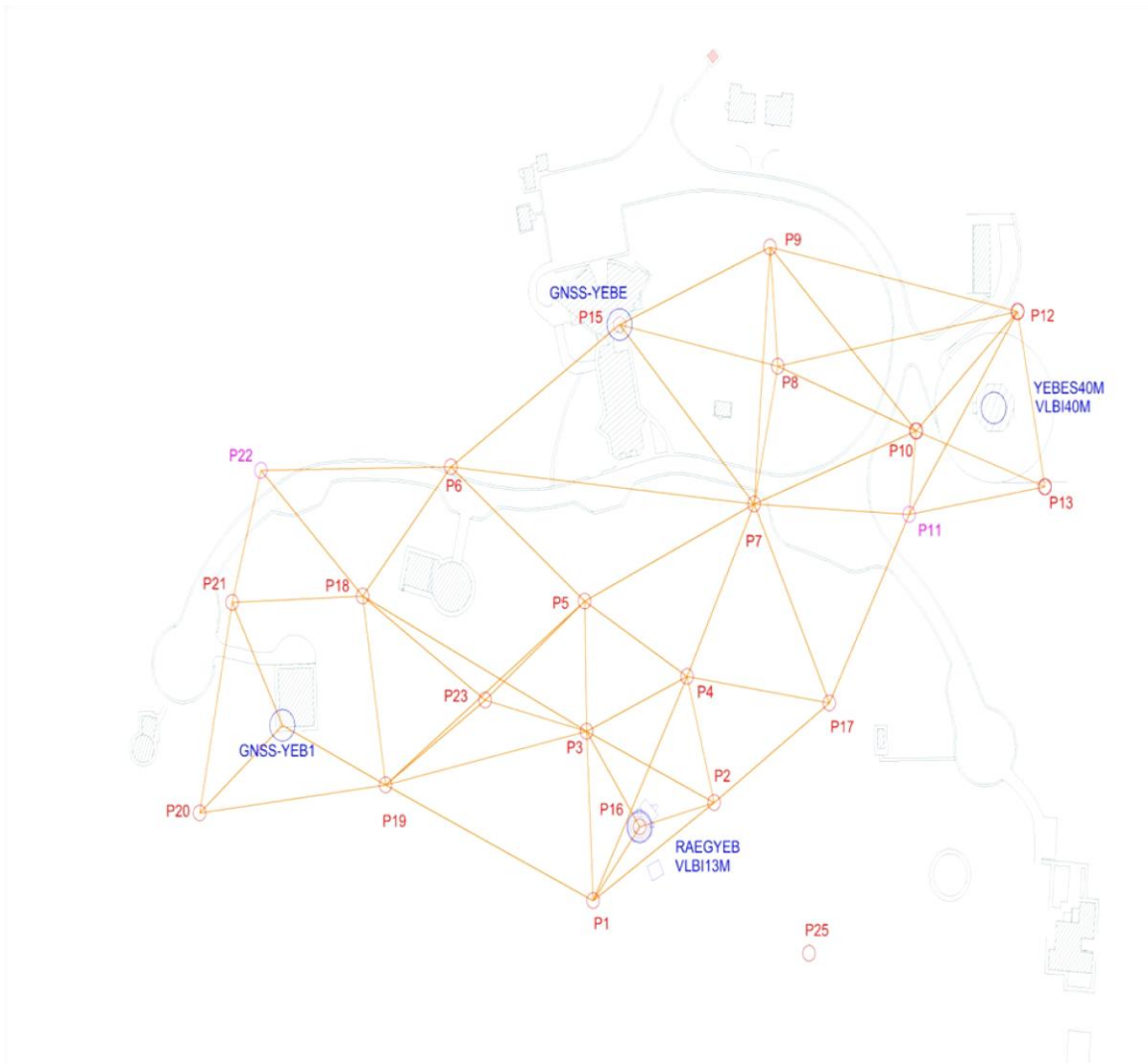


Figure 4.12

Name	DOMES number	Name in adjustment	Code	Description
P1	n/a	1	n/a	Auxiliary concrete pillar
P2	n/a	2	n/a	Auxiliary concrete pillar
P3	n/a	3	n/a	Auxiliary concrete pillar
P4	n/a	4	n/a	Auxiliary concrete pillar
P5	n/a	5	n/a	Auxiliary concrete pillar
P6	n/a	6	n/a	Auxiliary concrete pillar
P7	n/a	7	n/a	Auxiliary concrete pillar
P8	n/a	8	n/a	Auxiliary concrete pillar
P9	n/a	9	n/a	Auxiliary concrete pillar
P10	n/a	10	n/a	Auxiliary concrete pillar
P11	n/a	11	n/a	Reconstructed auxiliary concrete pillar
P12	n/a	12	n/a	Auxiliary concrete pillar
P13	n/a	13	n/a	Auxiliary concrete pillar
YEBES40M	13420S002	VLBI40m	7389	IRP of the 40m radiotelescope
P15	n/a	15	n/a	Planimetry IRP of the YEBE GNSS
YEBE	13420M001	YEBE	YEBE	IRP of the YEBE GNSS
P16	n/a	16	n/a	Central pillar inside the 13 m radiotelescope.
RAEGYEB	13420S003	VLBI13m	7386	IRP of the 13m radiotelescope
P17	n/a	17	n/a	Auxiliary concrete pillar
P18	n/a	18	n/a	Auxiliary concrete pillar
P19	n/a	19	n/a	Auxiliary concrete pillar
P20	n/a	20	n/a	Auxiliary concrete pillar
P21	n/a	21	n/a	Auxiliary concrete pillar
P22	n/a	22	n/a	Reconstructed auxiliary concrete pillar
P23	n/a	23	n/a	Auxiliary concrete pillar
YEB1	13420M002	YEB1	YEB1	IRP of the YEB1 GNSS
P25	n/a	-	n/a	Auxiliary concrete pillar not included in the network yet.

Table 4.12

4.5. SURVEY METHOD

4.5.1. GNSS MEASUREMENTS

Before the adjustment of the network is necessary having an approximate coordinates from which to start. With this purpose each pillar has been measured with a LEIAR20 GNSS antenna and a LEICA GR25 receiver during 5 hours. The YEBE IGS GNSS station was taken as reference point for all baselines.

To fix level and orientate the GNSS antenna a 8 cm SECO-MFG leveling platform were used. (Figure 4.13).



Figure 4.13

4.5.2. GROUND NETWORK SURVEY

The observation methodology of the network has been done with the resection with all possible angles and distances. Currently the leveling has been done using trigonometric methodology until we will get a level for more accurate slopes in the next future. It has been used the Leica TS50 total station with an accuracy of 0.5'' and 0.6 mm for angles and distances respectively.

The measurements were taken automatically using own software based on Leica Geocom commands, which controls the Total Station remotely through wire or Bluetooth (Figure 4.14). The methodology consists on doing 5 horizon turns, measuring each visual in direct circle (DC) and in inverse circle (IC).

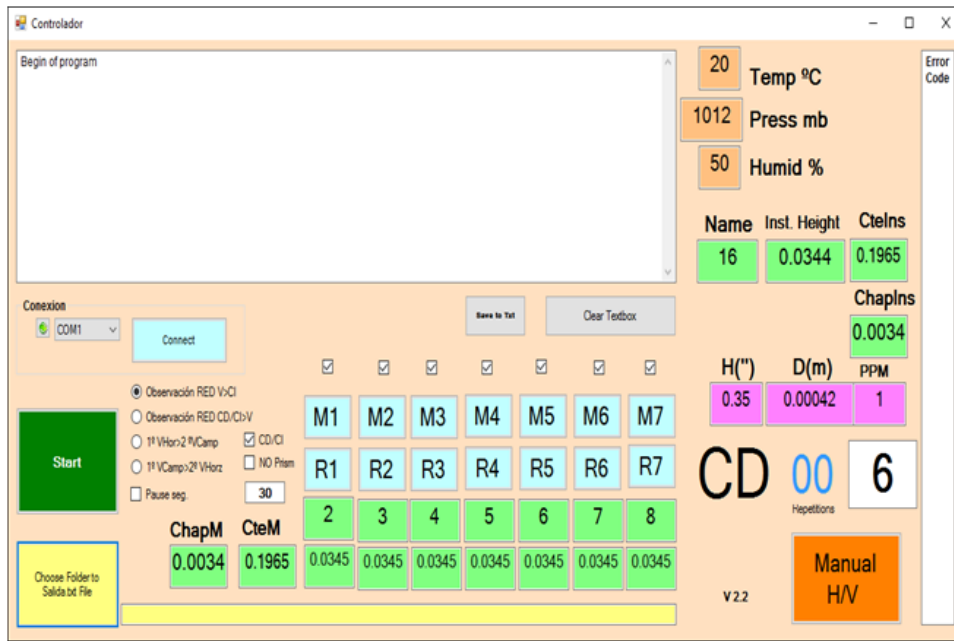


Figure 4.14

In each emplacement temperature, pressure and humidity have been measured and they have been introduced in the total station in order to do the appropriate corrections on to the angles and distances mainly produce by refraction. (Figure 4.15)



Figure 4.15

In each pillar, after placing tribachs, the height until the top of the screw, were the measurements are referenced, were measured. For this purpose was used a caliber and a plate of 3.4 mm width (Figure 4.16). These heights must be taken in to account to introduce the instrument height.



Figure 4.16



Figure 4.17



Figure 4.18

4.5.3. INVARIANT REFERENCE POINT

The Invariant Reference Point (IRP) is a theoretical point and it is defined as the intersection of the azimuth axis with the common perpendicular of the azimuth and elevation axis. It is the point from which the local tie is measured.

4.5.3.1. GNSS ANTENNAS

The IRP of a GNSS antenna is a point that lies on the main axis of symmetry of the antenna at a height that is determined in the specifications and usually coincides with the bottom of the antenna.

4.5.3.1.1. YEBE

Due to the importance and the fragility of this point the antenna could not be replaced by a reflector prism and the IRP was measured using direct intersection from pillars P6, P7, P8 and P9, creating a sub-network (Figure 4.19). The technique that has been used distinguishes between planimetry and altimetry.

To calculate the planimetry of the IRP, it was measured the axis of symmetry of the antenna using the cane that holds it, bisecting with the aiming wire of the total station.

The calculation of the altimetry was carried out pointing to the upper corner of the antenna from each of the pillars that surround it.



Figure 4.19

4.5.3.1.2. YEB1

In this case the methodology was easier because the antenna could be replaced by a GHP1 prism which was measured from each surrounded pillar. The sub-network that was used to measure the IRP is formed by the pillars P18, P19, P20 and P21. (Figure 4.20). From each of these pillars were taken measurements to the prism situated in the position of YEB1 and to the other pillars of the sub-network in order to orientate and re-force the network.

These data were added to the adjustment of the total network from which YEB1 was estimated.

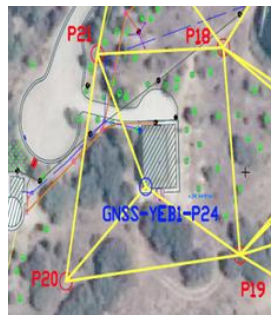


Figure 4.20

4.5.3.2. *RADIOTELESCOPES*

The IRP of a radio telescope is defined as the intersection between its azimuth axis and the elevation axis and in the case of non-intersection, is defined as the projection of the elevation axis on the azimuth axis. Usually this point is inaccessible or not materialized.

The used methodology to calculate it, has been the classic method of circles, which consists on the adjustment of measured points on the structure of the radio telescope under certain conditions or constraints to 3D circles. In this model the radio telescope is rotated around one of its axes leaving the other fixed, so that the trajectory of each marker corresponds to a circle. This process is repeated for different orientations of the radio telescope and for both axes.

4.5.3.2.1. RAEGEYEB-RADIOTELESCOPE

To calculate the IRP of the 13 meter radio telescope has been used two different methodologies: using a central pillar inside the cabin of the radio telescope and using external pillars which surrounded it.

4.5.3.2.1.1. *Using the central pillar*

In this case, IRP has been calculated placing the total station TS50 on the central pillar of the radio telescope (to which fixed coordinates of (1000, 2000, 3000) have been given) on a tripod integrated on the concrete tower of the radio telescope (Figure 4.21).



Figure 4.21

For a greater safety due to the limited space, the tripod was secured with flanges to the central pillar plate and raised high enough to allow visibility to the exterior pillars through two circular windows located in each of the counterweights allowing an inverse intersection from them (Figure 4.24).

The measurements were made by pointing to a corner cube reflector "RRR Hexagon", with a construction accuracy of 0.0001 mm, that was magnetically attached to the inside of both counterweights (Figures 4.22 and 4.23).



Figure 4.22



Figure 4.23

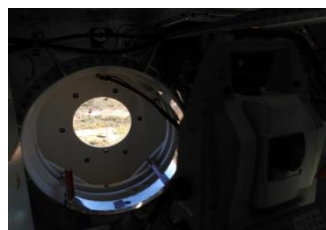


Figure 4.24

To perform the observation, the antenna was moved from 7° to 87° in elevation every 20° and from 0° to 360° in azimuth with a wait time between observations of 40 seconds.

Synchronized to the movement of the radio telescope, the total station was moved by tracking the prism and recording coordinates at every position of reflector prism RRR.

Once the measurements of the circles were finished, measurements were made to the exterior pillars to position the interior pillar of the cabin in the system of our network.

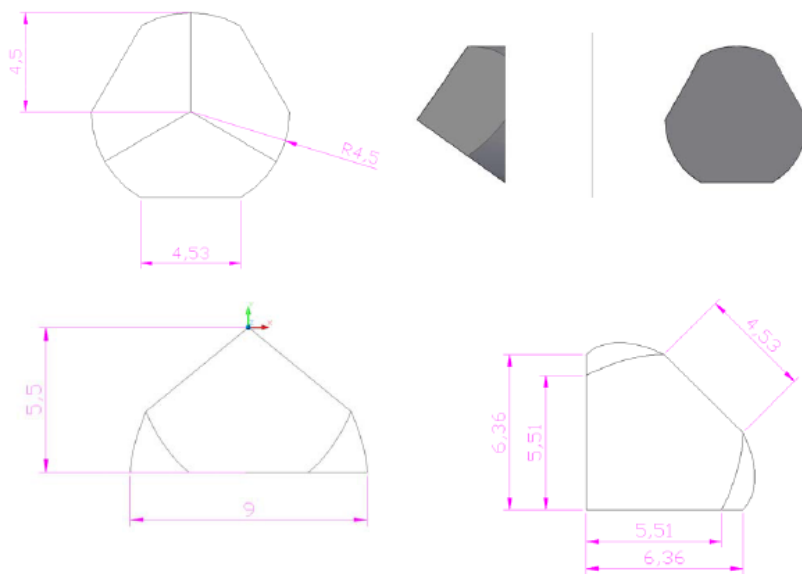
4.5.3.2.1.2. Using external pillars

In this case the IRP has been calculated from the outer pillars P1, P2 and P3 independently by making observations to two multi-prisms placed in the counterweights of the radio telescope. In this case the accuracy of the measurements is somewhat worse because the number of observations for each horizontal circle is reduced due to the lack of visibility from each pillar.

Each multi-prism (Figure 4.26), reflects the signal regardless of the angle at which they are viewed.

Each multiprism has been built in the Observatory using 4 corner cubes smaller of 1 cm and they have been glued to a magnet. Each corner cube was fabricated by an external optic company following the parameters of the Figure 4.25.

Parameters and technical drawing:



Material	N-BK7
Angles	+/- 3 arc secs Return Beam
Flatness	Lambda / 4
Dimension Tolerance	+ 0.00 / - 0.20mm
Surface Quality	60/40 Scratch-Dig
Coating to Entry Face	Uncoated
Coating to Reflective Surfaces	Aluminum & Black paint Protected
Diameter	9 mm
Height	5.50 mm
Straight length sides	4.53 mm
Wavelength to reflect	660 and 785 nm
Units of drawing	millimeters

Figure 4.25



Figure 4.26

4.5.3.2.2. YEBES40M-RADIOTELESCOPE

In the case of the 40 meter antenna it has only been possible to measure the IRP from the outer pillars to the radio telescope since there is no central pillar as in the case of the 13 meter

antenna. The methodology was therefore the same as for the calculation of the IRP of the 13-meter antenna, measuring two multi-prisms placed in the counterweights of the 40-meter antenna from three outer pillars with which to compare results. In this case the vertices from which it has been measured are P10, P12 and P13. In each of them a local system with fixed center (1000, 2000, 3000) was considered (Figure 4.27).



Figura 4.27

5. COMPUTATION

5.1. A PRIORI GROUND NETWORK COMPUTATION WITH GNSS.

In order to calculate a priori coordinates, each pillar was measured with GNSS as we have described in section 4.5.1. To calculate the coordinates X , Y , Z of each pillar and the matrix of covariance variances in the ETRS89 system it was used the software RTKLIB to calculate base lines with the reference station YEBE. The results were calculated using a static positioning mode, L1 carrier and an elevation mask of 10° . The estimated accuracy of the calculated coordinates was around 5 mm.

In Tables 5.1 and 5.2 are shown the a priori calculated coordinates X , Y , Z and the components of the matrix of variance and covariance.

Pillar	X	Y	Z
P1	4848838.46748804	-261648.839139577	4122952.44143507
P2	4848821.66560619	-261599.683776349	4122976.63512653
P3	4848809.1635627	-261648.541254706	4122989.04766349
P4	4848796.15866285	-261609.62171701	4123007.5543382
P5	4848779.00190937	-261649.095467739	4123026.13178675
P6	4848748.72661085	-261700.229575437	4123057.84038744
P7	4848764.06137227	-261579.168770024	4123047.40677275
P8	4848729.1712749	-261570.140406414	4123085.59266132
P9	4848705.96583733	-261572.217857121	4123110.48541736
P10	4848749.97420797	-261515.950059728	4123065.49343124
P11	4848767.45191657	-261519.12610301	4123046.47954681
P12	4848726.91225565	-261473.700467302	4123094.19388918
P13	4848762.95909663	-261463.75561826	4123052.6702999
P17	4848805.2407787	-261553.873025806	4123000.9917535
P18	4848772.65692897	-261737.855024411	4123028.60200104
P19	4848812.57529011	-261730.206234769	4122982.06609655
P20	4848812.44612257	-261800.368005395	4122976.31531809
P21	4848773.76384695	-261786.877460822	4123023.63874769
P22	4848745.04472608	-261776.001969224	4123057.58902675
P23	4848797.21159162	-261689.694742689	4123002.28820101

Table 5.1

Pillar	σ_x	σ_y	σ_z
P1	0.0021967664744783	0.00124719135701575	0.00156215438221639
P2	0.00261729097557773	0.00132518838428655	0.00251226976233565
P3	0.0019150983744192	0.00109495975739042	0.00157502156044411
P4	0.00225306927595032	0.00106735686630134	0.00136784629577462
P5	0.00235576789823201	0.00222055193935198	0.00731698975887661
P6	0.00262143827441235	0.00202810530902266	0.00312138518487508
P7	0.00351204944143924	0.00118207179332493	0.00389322709913218
P8	0.00191374607735515	0.00180097426462783	0.00274407912124309
P9	0.00265959222608829	0.00100510696737966	0.00136459840497499
P10	0.0056543588709386	0.00399232004534159	0.00230067157369263
P11	0.00443622344914938	0.0020951668287164	0.00453636910702778
P12	0.00649460201584733	0.00572858875364585	0.0108369142968034
P13	0.00954568486137456	0.00556871315446193	0.00450518110261332
P17	0.0037887385133709	0.00169952853862431	0.0025707998925698
P18	0.00174660287917168	0.00100440763489221	0.00149141218588193
P19	0.00667771215159946	0.0046414683508885	0.00693205649036649
P20	0.00356390444814925	0.0018502347709088	0.00250033158859858
P21	0.00939379739690801	0.00602603799346669	0.00705161193806246
P22	0.0046906477360767	0.00175768171542278	0.0032435533814584
P23	0.0028688938186512	0.00121334900907018	0.00163593747476464
Pillar	σ_{xy}	σ_{xz}	σ_{yz}
P1	-1.45408375895995E-06	2.28580826047188E-07	6.67913181145218E-07
P2	-2.29098588346398E-07	2.82602762403477E-06	1.22354053530804E-06
P3	-9.42252974444979E-07	4.49994084310835E-07	-1.6814551406918E-07
P4	-7.24038462815066E-07	1.03724953415546E-06	1.91983375102642E-07
P5	8.13971987606157E-07	7.93883462843094E-06	1.234655610335E-05
P6	-4.14909184029205E-06	5.46171627182901E-06	-4.44185964157222E-06
P7	1.05555634819988E-06	1.22508073969545E-05	1.12588069471562E-06
P8	-7.40218614526722E-07	1.86658562175175E-06	-3.67192951169507E-06
P9	2.46368127808443E-07	2.0760226843178E-06	-4.45209554951223E-08
P10	-1.11365486887935E-06	5.98924498838957E-06	3.74163601915279E-06
P11	-2.07726735033935E-06	1.13553213997044E-05	-9.85618163439743E-07
P12	-1.19806006149636E-05	4.76177588091475E-05	-9.25068465065346E-06
P13	4.52051236796396E-05	1.74172300426784E-05	3.15282291267426E-06
P17	1.45308948719966E-06	5.65199067105641E-06	2.06754186265518E-07
P18	-1.5584452772589E-07	1.1624380733851E-06	-2.3997662314702E-07
P19	-4.33711929776131E-06	1.68349903937159E-05	-2.77879323470346E-06
P20	4.69155198464283E-07	4.16587711513841E-06	-1.51499446707649E-06
P21	-3.34832411976026E-05	5.21382888796868E-05	-2.38276514542928E-05
P22	7.61638074223811E-07	1.00052708022447E-05	5.19621271425468E-07
P23	6.04051917867084E-07	3.30935938286857E-06	7.64088942257874E-07

Table 5.2

5.2. NETWORK SURVEY.

Once all measurements are taken and the IRP of the VLBI antennas and one of the GNSS antennas (YEBE) are calculated, the next step is to adjust the pillar network with all the measurements, including the sub-networks used to calculate the IRP of the radio telescopes of 13 and 40 meters and GNSS antennas. The adjustment has been made using GeoLabPX5 version 5.3.2. The input and output Geolab file are accessible in Annexes 3 and 4.

5.3. INVARIANT REFERENCE POINTS (IRPs).

5.3.1. GNSS.

Both YEB1 and planimetry of YEBE were adjusted with Geolab at the same time as the rest of the network. Altimetry of YEBE has been also calculated with Geolab taking into account just the height.

5.3.2. RADIO TELESCOPES.

The methodology to calculate the IRP of the radio telescopes, as in section 4.5.3.2 has been told is the classic method of circles, which consists on the adjustment of measured points on the structure of the radio telescope under certain conditions or constraints to 3D circles and arcs.

Once all the measurements have been taken, the computation that has been carried on is summarized here.

Firstly the azimuth axis is calculated. For this purpose are used observations to a prism during the rotation of the radio telescope around the azimuth axis for different elevations.

Secondly elevation axes are calculated for which observations are made to a prism during the rotation of the radio telescope around the axes of elevation for different azimuths. The centers of the arcs adjusted together with the normal vector of each arc of circumference generate the axes of elevation.

Observations are adjusted to circles in space (intersection between a sphere and a plane), taking into account in addition that the center of the sphere must satisfy the equation of the plane. In the setting, the parameters of each circumference (center and radius) are determined.

The adjustment equations are:

Sphere:

$$F(L, X) = (x_i - a)^2 + (y_i - b)^2 + (z_i - c)^2 - r^2$$

Plane:

$$G(L, X) = A \cdot x_i + B \cdot y_i + C - z_i$$

Constrains:

$$H(L, X) = A \cdot a + B \cdot b + C - c$$

where (a, b, c) , r are the center and the radius of the sphere, and A, B, C are the plane parameters.

5.3.2.1. RAEGEYEB-RADIOTELESCOPE

Here are shown the computations that have been done with both methodologies: using a central pillar inside the cabin of the radio telescope and using the external pillars which surrounded it.

5.3.2.1.1. Using the central pillar

An example of the adjusted horizontal circles and vertical arcs are shown in Figures 5.1 and 5.2:

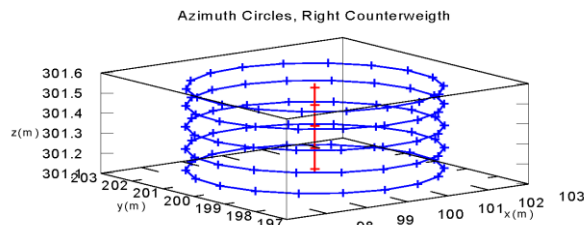


Figura 5.1

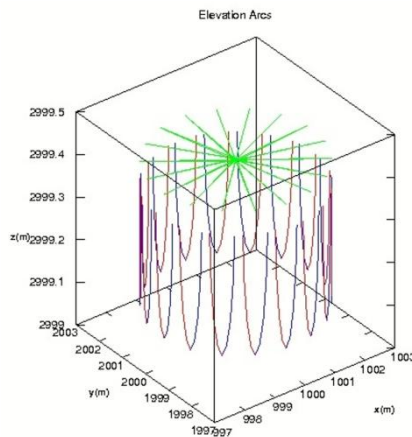


Figura 5.2

Table 5.3 shows the coordinates obtained of the P1, P2 and P3 pillars from the interior of the cab in the local coordinate system with an arbitrary center system (1000, 2000, 3000).

	x	y	Z	σ_x	σ_y	σ_z
P1	978.846658	2020.871601	2990.070556	0.000074	0.000148	0.000071
P2	1004.480675	1969.629860	2991.011311	0.000135	0.000093	0.000021
P3	1025.557567	2017.089360	2991.589699	0.000043	0.000068	0.000071

Table 5.3

5.3.2.1.2. Using the external pillars

An example of the vertical and horizontal circle arcs for both counterweights from one of the pillars can be seen in Figures 5.3, 5.4 and 5.5.

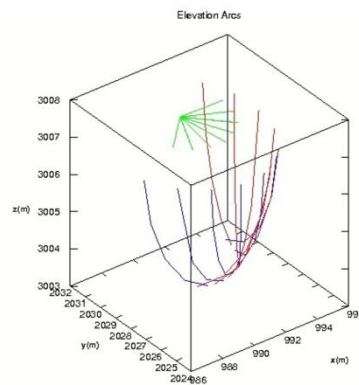


Figura 5.3

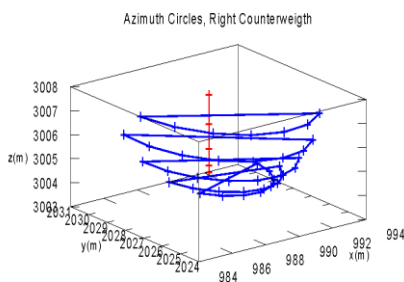


Figura 5.4

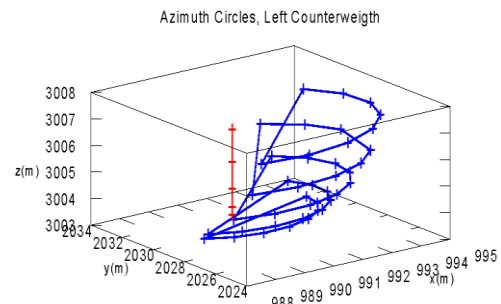


Figura 5.5

From each vertex the IRP of the radiotelescope has been calculated in a different local system. On each pillars an arbitrary system with fixed center (1000, 2000, 3000) was considered.

5.3.2.1.3. Results

All the calculations made have been verified with the AXIS program reaching similar results. In Table 5.4 we can see a summary of all the invariant points calculated by the different methodologies in their local systems.

	IRPs RAEGEYEB radio telescope			Eccentricity (m)
	x (m)	y (m)	z (m)	
INSIDE THE CAB	999.995744 ±0.000005	1999.985069 ±0.000004	2999.4148 ±0.0004	0.0015±0.0008
FROM P1	1016.9103 ±0.0006	2024.4467 ±0.0003	3009.1247 ±0.0007	0.0021±0.0009
FROM P2	991.7959 ±0.0007	1970.4331 ±0.0005	3008.1757 ±0.0009	0.0019±0.0011
FROM P3	990.2755 ±0.0006	2029.1783 ±0.0012	3007.5961 ±0.0018	0.0014±0.0016

Table 5.4

Also the measurement of the 13 and 40 meters radiotelescope IRPs from external pillars have been useful to study the accuracy and validate the use of the multi-prism technique. For this purpose, a study of the residuals of the adjusted circles data from the different pillars has been made getting residuals below 1mm in the adjustment of horizontal circles.

5.3.2.2. YEBES40M-RADIOTELESCOPE

In Table 5.5 it can be seen all the calculated IRPs from the different pillars in their arbitrary local systems:

	IRPs YEBES40M radio telescope			Eccentricity (m)
	x (m)	y (m)	z (m)	
FROM P10	1031.587±0.002	1990.7866±0.0007	3020.280±0.002	2.005±0.005
FROM P12	989.8568±0.0009	1969.9515±0.0005	3020.8831±0.0018	2.005±0.003
FROM P13	970.1790±0.0012	1988.57344±0.0004	3020.9055±0.0016	2.007±0.003

Table 5.5

5.4. IRP FROM RADIOTELESCOPES INTO THE GEOCENTRIC NETWORK SYSTEM TRANSFORMATION

Both the IRP of the 13-meter radio telescope and the 40-meter radio telescope are given in their respective local systems. To transform both points into the geocentric network system it is necessary to make 7-parameter Helmert 3D transformations, composed of three translations, three turns and a scale factor. Thus, from several points given in both systems (at least three), any point of a system can be transformed into the other system.

In addition, this transformation, carried out by an own matlab software, has allowed us to compare, in the case of radio telescopes, the IRPs calculated from the different pillars. In these cases the pillars are given both in the geocentric network system and in the local system in which the measurements of the IRP are calculated, since at least two other pillars were measured from this position.

5.4.1. RAEGEYEB-RADIOTELESCOPE

The IRPs in the case of the 13-meter antenna in the geocentric network system obtained from the Helmert transformation are shown in Table 5.6:

IRPs RAEGEYEB radio telescope (Geocentric network system)			
	X (m)	Y (m)	Z (m)
Inside the cab	4848831.4580± 0.0003	-261629.951531± 0.000017	4122976.2154± 0.0003
From P1	4848831.4573± 0.0005	-261629.9503± 0.0006	4122976.2150± 0.0005
From P2	4848831.4583± 0.0008	-261629.9509± 0.0006	4122976.2160± 0.0008
From P3	4848831.4575± 0.0016	-261629.9518± 0.0007	4122976.2158± 0.0015

Table 5.6

In order to calculate the 13 meters radiotelescope IRP from outside, the average of the points obtained from the three external vertices P1, P2 and P3 (Table 5.7) was performed.

IRPs RAEGEYEB radio telescope (Geocentric network system)			
	X (m)	Y (m)	Z (m)
Inside the cab	4848831.4580± 0.0003	-261629.951531± 0.000017	4122976.2154± 0.0003
Average P1P2P3	4848831.4577±0.0005	-261629.9510±0.0008	4122976.2156±0.0005
Difference interior-exterior the cabin.	0.0003	0.0005	0.0002

Table 5.7

These data reflect a great kindness in the adjustment using the measurements made from the three outer pillars with the multi-prism.

5.4.2. YEBES40M -RADIOTELESCOPE

The IRPs in the case of the 40-meter radio telescope obtained in the geocentric network system from the 3D Helmert transformation, as well as the mean values obtained from pillars P10, P12 and P13 are shown in Table 5.8.

IRPs YEBES40M radio telescope (Geocentric network system)			
	X (m)	Y (m)	Z (m)
From P10	4848762.1745±0.0017	-261484.6063±0.0018	4123084.7793±0.0016
From P12	4848762.1773±0.0014	-261484.6087±0.0009	4123084.7781±0.0012
From P13	4848762.1760±0.0014	-261484.6080±0.0005	4123084.7816±0.0014
Average P10P12P13	4848762.1759± 0.0014	-261484.6076±0.0012	4123084.7796±0.0018

Table 5.8

5.5. IMPORTING INVARIANTE REFERENCE POINTS INTO TOPOMETRIC COMPUTATION

Once the IRPs of the different techniques and the adjusted network have been calculated, it is necessary to connect these points with the rest of the local network. This work has been carried out with Geolab software, radiating the differences of distances between pillar and IRP (DX, DY, DZ), from the pillars from which these IRPs have been measured and whose coordinates are known in the geocentric network system. The IRP integrated in the network as well as their variance covariance matrix are shown in Table 5.9.

```

* Number of degrees of freedom of adjustment = 2044
* Number of stations in adjusted network = 27
* Number of stations extracted = 4
*
3DC
XYZ VLBI40m 4848762.175895 -261484.607603 4123084.779600 m 0
XYZ VLBI13m 4848831.457742 -261629.951571 4122976.215159 m 0
XYZ YEBE 4848724.984533 -261632.472188 4123093.985476 m 0
XYZ YEB1 4848800.499013 -261769.654085 4123001.164204 m 0
COV CT UPPR
ELEM 2.04995928339998e-06 7.16283500023397e-09 3.1452196037248e-08
ELEM 2.81335704572559e-07 -6.91525408039266e-08 8.75753167791391e-08
ELEM 3.05526699759183e-07 1.69516980533409e-08 8.17964690560368e-08
ELEM 2.24703679820563e-07 -4.43249273950196e-08 1.54269074606231e-07
ELEM 1.36727295139055e-06 -4.22290921817372e-08 -2.19529302138495e-08
ELEM 4.74386940699216e-08 -1.20160430429116e-08 -1.34324125046242e-08
ELEM 1.12748587668803e-07 -1.87858075530456e-08 -5.40408539776911e-08
ELEM 6.22848744968344e-08 2.5944409203196e-08
ELEM 3.06137011901663e-06 9.3768488574705e-08 4.54412340251479e-08
ELEM 1.82919763040765e-07 8.09658039222677e-08 -5.57605744271311e-08
ELEM 2.04800468550067e-07 1.59617100649855e-07 1.62826807095491e-08
ELEM 1.04283238378311e-07
ELEM 3.78593428284535e-07 -3.61090986308904e-08 9.57092626539788e-08
ELEM 2.78464367188601e-07 -4.14028673559747e-08 9.47962129978466e-08
ELEM 2.72281713474728e-07 1.78777800157107e-08 1.17035042106254e-07
ELEM 2.02816254020516e-07 1.19926186566851e-08 -2.18861582964578e-08
ELEM 4.10368754150812e-08 -1.48256949858608e-08 -3.01058728796443e-08
ELEM 9.51458726324386e-08 1.72376914062188e-09
ELEM 2.6869471449628e-07 9.78992062976158e-08 1.27358119889668e-08
ELEM 1.75699736776599e-07 1.10524801757909e-07 -5.24431562104514e-08
ELEM 1.55897878476783e-07
ELEM 4.06079916628841e-07 -1.21485763775982e-08 9.36084279825302e-08
ELEM 2.58421692040105e-07 -3.20421607374693e-08 1.19683110070407e-07
ELEM 2.31255716722584e-07 -2.20597058197717e-08 -6.38979587785491e-08
ELEM 6.1043292203574e-08 3.48713593179878e-08
ELEM 2.7956390285999e-07 1.22603324421109e-07 1.60471673280528e-09
ELEM 1.47220120120083e-07
ELEM 4.18854466536725e-07 -6.06358036832281e-09 3.025026384487e-08
ELEM 1.73967777537483e-07 -2.6003745015791e-08
ELEM 3.23591473262172e-07
*
* End of extracted coordinates
*

```

Table 5.9

5.6. TRANSFORMATION INTO IGB08

Finally, it is necessary to transform the IRPs of the geocentric network system into an international global system. In our case we will transform them into the IGB08 international system. For this purpose, the data of three GNSS stations measuring permanently located in the Observatory have been taken in order to be able to perform a 7-parameter Helmert transformation. The used stations have been YEBE, YEB1 and a GNSS LEIAR20 antenna with a LEICA GR25 receiver located on Pillar 17 which has an enough long series of data to be able to carry out this task. Through these data BERNESE coordinates have been calculated in the IGB08 system of these three points using baselines with stations around the world to achieve enough accuracy (these results have been obtained by the IGN calculation center). Taking into account that the coordinates of these three points in the network system are also known we can obtain the parameters of the Helmert transformation between both systems, for which the scale factor has been set to 1.

The processed coordinates with Bernesse for YEBE, YEB1 and Pillar 17 in the IGB08 system are shown in Table 5.10, while the coordinates in the geocentric network system are shown in Table 5.11.

Estación	X (IGb08)	Y(IGb08)	Z(IGb08)
Pilar 17	4848804.8459±0.0009	-261553.3745±0.0006	4123001.3083±0.0012
GNSS YEB1(P24)	4848800.0727±0.0011	-261769.1554±0.0004	4123001.4531±0.0017
GNSS YEBE	4848724.5962±0.0007	-261631.9794±0.0003	4123094.3037±0.0008

Table 5.10

Estación	X (Local)	Y (Local)	Z (Local)
Pilar 17	4848805.241667±0.0006	-261553.870961±0.0003	4123000.994858±0.0005
GNSS YEB1(P24)	4848800.453498±0.0006	-261769.651635±0.0004	4123001.125186±0.0006
GNSS YEBE	4848724.984574±0.0006	-261632.472593±0.0004	4123093.985536±0.0005

Table 5.11

The IRPs that must be transformed are given in Table 5.12.

Estación	X (Local)	Y (Local)	Z (Local)
YEB1	4848800.4991±0.0007	-261769.6541±0.0004	4123001.1641±0.0006
VLBI13m	4848831.4580± 0.0003	-261629.9553±0.000017	4122976.2154± 0.0003
VLBI40m	4848762.1758± 0.0014	-261484.6076±0.0012	4123084.7796±0.0018
YEBE	4848724.9845± 0.0004	-261632.4726±0.0006	4123093.9855±0.0005

Table 5.12

The transformed parameters as well as the transformed IRP in the IGB08 system are found in Tables 5.13 and 5.14.

S:	1.000000	sigma	0.000000		
Giro1(°):	359.997420	sigma(°)	0.000767	sigma(")	2.760278
Giro2(°):	0.000714	sigma(°)	0.001120	sigma(")	4.030657
Giro3(°):	0.004569	sigma(°)	0.000745	sigma(")	2.683528
Tx(m):	-0.388313	sigma(m)	0.001169		
Ty(m):	0.495296	sigma(m)	0.000661		
Tz(m):	0.319840	sigma(m)	0.001366		

Table 5.13

Pilar	X	SX	Y	SY	Z	SZ
YEB1	4848800.120060	0.000632	-261769.158390	0.000414	4123001.488133	0.000552
VLBI13m	4848831.067509	0.000594	-261629.454477	0.000425	4122976.532356	0.000497
VLBI40m	4848761.775169	0.001409	-261484.111184	0.001240	4123085.091274	0.001811
YEBE	4848724.595679	0.000565	-261631.978731	0.000434	4123094.304297	0.000488

Table 5.14

6. RESULTS

6.1. ADJUSTED COORDINATES.

The results of the adjustment are the coordinates of all points as well as their standard deviation in the IGS08 frame at the mean epoch of the observations (i.e. epoch 2016.90). Hereafter is a table with the Geocentric coordinates and the standard deviation of all the points of the network (Table 6.1).

Pillar	X	Y	Z
P1	4848838.0840±0.0005	-261648.3427±0.0004	4122952.7665±0.0004
P2	4848821.2685±0.0006	-261599.1896±0.0003	4122976.9502±0.0005
P3	4848808.7742±0.0005	-261648.0443±0.0003	4122989.3639±0.0004
P4	4848795.7651±0.0005	-261609.1246±0.0003	4123007.8712±0.0004
P5	4848778.6010±0.0005	-261648.5998±0.0003	4123026.4422±0.0004
P6	4848748.3416±0.0005	-261699.7343±0.0003	4123058.1586±0.0004
P7	4848763.6733±0.0005	-261578.6769±0.0003	4123047.7255±0.0004
P8	4848728.7751±0.0006	-261569.64488±0.0004	4123085.9031±0.0005
P9	4848705.5702±0.0006	-261571.7228±0.0004	4123110.8005±0.0005
P10	4848749.5747±0.0006	-261515.4558±0.0004	4123065.8057±0.0005
P11	4848767.0484±0.0006	-261518.6281±0.0003	4123046.7913±0.0005
P12	4848726.5027±0.0006	-261473.2082±0.0004	4123094.4900±0.0006
P13	4848762.5432±0.0006	-261463.2641±0.0004	4123052.9786±0.0006
P16	4848831.5093±0.0006	-261629.4934±0.0004	4122976.9150±0.0005
P17	4848804.8455±0.0006	-261553.3749±0.0003	4123001.3092±0.0005
P18	4848772.2773±0.0006	-261737.3613±0.0003	4123028.9230±0.0005
P19	4848812.1799±0.0006	-261729.7089±0.0003	4122982.3708±0.0005
P20	4848812.0669±0.0006	-261799.8688±0.0004	4122976.6310±0.0006
P21	4848773.3839±0.0006	-261786.3797±0.0003	4123023.9553±0.0005
P22	4848744.6577±0.0006	-261775.5086±0.0004	4123057.9131±0.0005
P23	4848796.8288±0.0006	-261689.2011±0.0003	4123002.6099±0.0004
YEB1	4848800.1199±0.0006	-261769.1584±0.0004	4123001.4882±0.0006
VLBI13m	4848831.0675±0.0006	-261629.4545±0.0004	4122976.5324±0.0005
VLBI40m	4848761.7752±0.0014	-261484.1112±0.0012	4123085.0913±0.0018
YEBE	4848724.5957±0.0006	-261631.9787±0.0004	4123094.3043±0.0005

Table 6.1

The whole covariance matrix was computed. It was possible to extract from it the covariance submatrix for the following points of interest: YEB1, VLBI13m, VLBI40m and YEBE. This covariance submatrix has been converted into the SINEX format with an own matlab software. The resulting SINEX file (13420_IGN_2017-117.snx) is given in Annex 5.

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Annex 2: YEB1 GNSS station



Área de Geodesia
Subdirección General de Geodesia y Cartografía

Reseña de Estación Permanente - ERGNSS

4-mar-2017

Situación:

Código.....: **YEB1** Municipio: Yebes
Nombre.....: **Yebes 1**
Código IERS: 13420M002 Provincia: Guadalajara
Instalación...: 22 de abril de 2009

Localización.: Guadalajara
Centro Astronómico de Yebes, Aptdo. 143, 19080 - Guadalajara

Construcción: Pilar de hormigón armado de 1.2 m de altura.
Marca de coordenadas, parte superior sobre placa metálica.

Coordenadas ETRS89:

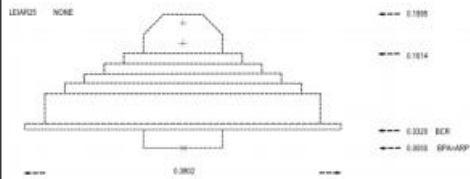
Longitud.....: - 3° 05' 24,71087"	X.....: 4848800.403 m
Latitud.....: 40° 31' 25,60071"	Y.....: -261769.653 m
Altitud elipsoidal: 975.367 m.	Z.....: 4123001.077 m.
X UTM.....: 492359.920 m.	Altitud sobre el nivel medio del mar:
Y UTM.....: 4485897.996 m.	
Huso.....: 30	923.378 m.



Instrumentación:

Receptor: GRX1200+GNSS
Antena: LEIAR25 NONE Altura: 0.0600 m. (ARP)
Offset de centros de fase de antena: L1 0.155 m. L2 0.164 m.

Esquema antena



Información adicional:

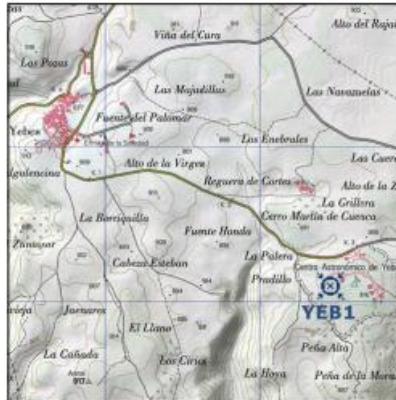
Esta estación permanente pertenece a la red ERGNSS.

Datos horarios a 1, 5, 15 y 30 segundos y diarios a 30 segundos
<http://ftp.geodesia.ign.es>

Emite correcciones diferenciales a través del Caster <http://ernss-ig.ign.es>
a través de los puntos de montaje:

- YEB10 formato de la corrección RTCM versión RTCM 3.1
- YEB11 formato de la corrección RTCM versión RTCM 2.3

E-mail de contacto: buzon-geodesia@fomento.es



Observaciones:

Empty box for observations.

000	3	5	150 34 28.7183	000	21	0.2381	0.13	000	28	0.2383	0.13
000	3	10	244 14 21.2141	000	20	0.2380	0.13	000	27	0.2382	0.13
000	3	15	204 24 20.0151	000	19	0.2379	0.13	000	26	0.2381	0.13
000	3	20	50 0 19.8161	000	18	0.2378	0.13	000	25	0.2380	0.13
000	3	25	150 14 18.6171	000	17	0.2377	0.13	000	24	0.2379	0.13
000	3	30	244 14 17.4181	000	16	0.2376	0.13	000	23	0.2378	0.13
000	3	35	338 14 16.2191	000	15	0.2375	0.13	000	22	0.2377	0.13
000	3	40	432 14 15.0201	000	14	0.2374	0.13	000	21	0.2376	0.13
000	3	45	526 14 13.8211	000	13	0.2373	0.13	000	20	0.2375	0.13
000	3	50	620 14 12.6221	000	12	0.2372	0.13	000	19	0.2374	0.13
000	3	55	714 14 11.4231	000	11	0.2371	0.13	000	18	0.2373	0.13
000	3	60	808 14 10.2241	000	10	0.2370	0.13	000	17	0.2372	0.13
000	3	65	902 14 9.0251	000	9	0.2369	0.13	000	16	0.2371	0.13
000	3	70	996 14 7.8261	000	8	0.2368	0.13	000	15	0.2370	0.13
000	3	75	1090 14 6.6271	000	7	0.2367	0.13	000	14	0.2369	0.13
000	3	80	1184 14 5.4281	000	6	0.2366	0.13	000	13	0.2368	0.13
000	3	85	1278 14 4.2291	000	5	0.2365	0.13	000	12	0.2367	0.13
000	3	90	1372 14 3.0301	000	4	0.2364	0.13	000	11	0.2366	0.13
000	3	95	1466 14 1.8311	000	3	0.2363	0.13	000	10	0.2365	0.13
000	3	100	1560 14 0.6321	000	2	0.2362	0.13	000	9	0.2364	0.13
000	3	105	1654 14 0.4331	000	1	0.2361	0.13	000	8	0.2363	0.13
000	3	110	1748 14 0.2341	000	0	0.2360	0.13	000	7	0.2362	0.13
000	3	115	1842 14 0.0351	000	0	0.2359	0.13	000	6	0.2361	0.13
000	3	120	1936 14 0.8361	000	0	0.2358	0.13	000	5	0.2360	0.13
000	3	125	2030 14 0.6371	000	0	0.2357	0.13	000	4	0.2359	0.13
000	3	130	2124 14 0.4381	000	0	0.2356	0.13	000	3	0.2358	0.13
000	3	135	2218 14 0.2391	000	0	0.2355	0.13	000	2	0.2357	0.13
000	3	140	2312 14 0.0401	000	0	0.2354	0.13	000	1	0.2356	0.13
000	3	145	2406 14 0.8411	000	0	0.2353	0.13	000	0	0.2355	0.13
000	3	150	2500 14 0.6421	000	0	0.2352	0.13	000	0	0.2354	0.13
000	3	155	2594 14 0.4431	000	0	0.2351	0.13	000	0	0.2353	0.13
000	3	160	2688 14 0.2441	000	0	0.2350	0.13	000	0	0.2352	0.13
000	3	165	2782 14 0.0451	000	0	0.2349	0.13	000	0	0.2351	0.13
000	3	170	2876 14 0.8461	000	0	0.2348	0.13	000	0	0.2350	0.13
000	3	175	2970 14 0.6471	000	0	0.2347	0.13	000	0	0.2349	0.13
000	3	180	3064 14 0.4481	000	0	0.2346	0.13	000	0	0.2348	0.13
000	3	185	3158 14 0.2491	000	0	0.2345	0.13	000	0	0.2347	0.13
000	3	190	3252 14 0.0501	000	0	0.2344	0.13	000	0	0.2346	0.13
000	3	195	3346 14 0.8511	000	0	0.2343	0.13	000	0	0.2345	0.13
000	3	200	3440 14 0.6521	000	0	0.2342	0.13	000	0	0.2344	0.13
000	3	205	3534 14 0.4531	000	0	0.2341	0.13	000	0	0.2343	0.13
000	3	210	3628 14 0.2541	000	0	0.2340	0.13	000	0	0.2342	0.13
000	3	215	3722 14 0.0551	000	0	0.2339	0.13	000	0	0.2341	0.13
000	3	220	3816 14 0.8561	000	0	0.2338	0.13	000	0	0.2340	0.13
000	3	225	3910 14 0.6571	000	0	0.2337	0.13	000	0	0.2339	0.13
000	3	230	4004 14 0.4581	000	0	0.2336	0.13	000	0	0.2338	0.13
000	3	235	4098 14 0.2591	000	0	0.2335	0.13	000	0	0.2337	0.13
000	3	240	4192 14 0.0601	000	0	0.2334	0.13	000	0	0.2336	0.13
000	3	245	4286 14 0.8611	000	0	0.2333	0.13	000	0	0.2335	0.13
000	3	250	4380 14 0.6621	000	0	0.2332	0.13	000	0	0.2334	0.13
000	3	255	4474 14 0.4631	000	0	0.2331	0.13	000	0	0.2333	0.13
000	3	260	4568 14 0.2641	000	0	0.2330	0.13	000	0	0.2332	0.13
000	3	265	4662 14 0.0651	000	0	0.2329	0.13	000	0	0.2331	0.13
000	3	270	4756 14 0.8661	000	0	0.2328	0.13	000	0	0.2330	0.13
000	3	275	4850 14 0.6671	000	0	0.2327	0.13	000	0	0.2329	0.13
000	3	280	4944 14 0.4681	000	0	0.2326	0.13	000	0	0.2328	0.13
000	3	285	5038 14 0.2691	000	0	0.2325	0.13	000	0	0.2327	0.13
000	3	290	5132 14 0.0701	000	0	0.2324	0.13	000	0	0.2326	0.13
000	3	295	5226 14 0.8711	000	0	0.2323	0.13	000	0	0.2325	0.13
000	3	300	5320 14 0.6721	000	0	0.2322	0.13	000	0	0.2324	0.13
000	3	305	5414 14 0.4731	000	0	0.2321	0.13	000	0	0.2323	0.13
000	3	310	5508 14 0.2741	000	0	0.2320	0.13	000	0	0.2322	0.13
000	3	315	5602 14 0.0751	000	0	0.2319	0.13	000	0	0.2321	0.13
000	3	320	5696 14 0.8761	000	0	0.2318	0.13	000	0	0.2320	0.13
000	3	325	5790 14 0.6771	000	0	0.2317	0.13	000	0	0.2319	0.13
000	3	330	5884 14 0.4781	000	0	0.2316	0.13	000	0	0.2318	0.13
000	3	335	5978 14 0.2791	000	0	0.2315	0.13	000	0	0.2317	0.13
000	3	340	6072 14 0.0801	000	0	0.2314	0.13	000	0	0.2316	0.13
000	3	345	6166 14 0.8811	000	0	0.2313	0.13	000	0	0.2315	0.13
000	3	350	6260 14 0.6821	000	0	0.2312	0.13	000	0	0.2314	0.13
000	3	355	6354 14 0.4831	000	0	0.2311	0.13	000	0	0.2313	0.13
000	3	360	6448 14 0.2841	000	0	0.2310	0.13	000	0	0.2312	0.13
000	3	365	6542 14 0.0851	000	0	0.2309	0.13	000	0	0.2311	0.13
000	3	370	6636 14 0.8861	000	0	0.2308	0.13	000	0	0.2310	0.13
000	3	375	6730 14 0.6871	000	0	0.2307	0.13	000	0	0.2309	0.13
000	3	380	6824 14 0.4881	000	0	0.2306	0.13	000	0	0.2308	0.13
000	3	385	6918 14 0.2891	000	0	0.2305	0.13	000	0	0.2307	0.13
000	3	390	7012 14 0.0901	000	0	0.2304	0.13	000	0	0.2306	0.13
000	3	395	7106 14 0.8911	000	0	0.2303	0.13	000	0	0.2305	0.13
000	3	400	7200 14 0.6921	000	0	0.2302	0.13	000	0	0.2304	0.13
000	3	405	7294 14 0.4931	000	0	0.2301	0.13	000	0	0.2303	0.13
000	3	410	7388 14 0.2941	000	0	0.2300	0.13	000	0	0.2302	0.13
000	3	415	7482 14 0.0951	000	0	0.2299	0.13	000	0	0.2301	0.13
000	3	420	7576 14 0.8961	000	0	0.2298	0.13	000	0	0.2299	0.13
000	3	425	7670 14 0.6971	000	0	0.2297	0.13	000	0	0.2298	0.13
000	3	430	7764 14 0.4981	000	0	0.2296	0.13	000	0	0.2297	0.13
000	3	435	7858 14 0.2991	000	0	0.2295	0.13	000	0	0.2296	0.13
000	3	440	7952 14 0.1001	000	0	0.2294	0.13	000	0	0.2295	0.13
000	3	445	8046 14 0.9011	000	0	0.2293	0.13	000	0	0.2294	0.13
000	3	450	8140 14 0.7021	000	0	0.2292	0.13	000	0	0.2293	0.13
000	3	455	8234 14 0.5031	000	0	0.2291	0.13	000	0	0.2292	0.13
000	3	460	8328 14 0.3041	000	0	0.2290	0.13	000	0	0.2291	0.13
000	3	465	8422 14 0.1051	000	0	0.2289	0.13	000	0	0.2290	0.13
000	3	470	8516 14 0.9061	000	0	0.2288	0.13	000	0	0.2289	0.13
000	3	475	8610 14 0.7071	000	0	0.2287	0.13	000	0	0.2288	0.13
000	3	480	8704 14 0.5081	000	0	0.2286	0.13	000	0	0.2287	0.13
000	3	485	8798 14 0.3091	000	0	0.2285	0.13	000	0	0.2286	0.13
000	3	490	8892 14 0.1101	000	0	0.2284	0.13	000	0	0.2285	0.13
000	3	495	8986 14 0.9111	000	0	0.2283	0.13	000	0	0.2284	0.13
000	3	500	9080 14 0.7121	000	0	0.2282	0.13	000	0	0.2283	0.13
000	3	505	9174 14 0.5131	000	0	0.2281	0.13	000	0	0.2282	0.13
000	3	510	9268 14 0.3141	000	0	0.2280	0.13	000	0	0.2281	0.13
000	3	515	9362 14 0.1151	000	0	0.2279	0.13	000	0	0.2280	0.13
000	3	520	9456 14 0.9161	000	0	0.2278	0.13	000	0	0.2279	0.13
000	3	525	9550 14 0.7171	000	0	0.2277	0.13	000	0	0.2278	0.13
000	3	530	9644 14 0.5181	000	0	0.2276	0.13	000	0	0.2277	0.13
000	3	535	9738 14 0.3191	000	0	0.2275	0.13	000	0	0.2276	0.13
000	3	540	9832 14 0.1201	000	0	0.2274	0.13	000	0	0.2275	0.13
000	3	545									

DMMO VWR 7	10	91 18 01377	0.13	WY	DMMO VWR 11	11	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	2	54.424753	m	
DMMO VWR 7	11	0.2302 4	90 27 15.9749	0.13	WY	DMMO VWR 12	12	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	3	48.584824	m
DMMO VWR 7	12	0.2302 4	90 27 15.9749	0.13	WY	DMMO VWR 13	13	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	4	42.744895	m
DMMO VWR 7	13	0.2302 4	89 40 40.8038	0.13	WY	DMMO VWR 14	14	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	5	36.904966	m
DMMO VWR 7	14	0.2302 4	89 40 40.8038	0.13	WY	DMMO VWR 15	15	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	6	31.065037	m
DMMO VWR 7	15	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 16	16	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	7	25.225108	m
DMMO VWR 7	16	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 17	17	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	8	19.385179	m
DMMO VWR 7	17	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 18	18	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	9	13.545250	m
DMMO VWR 7	18	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 19	19	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	10	7.705321	m
DMMO VWR 7	19	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 20	20	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	11	1.865392	m
DMMO VWR 7	20	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 21	21	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	12	-4.074639	m
DMMO VWR 7	21	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 22	22	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	13	-10.014690	m
DMMO VWR 7	22	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 23	23	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	14	-15.954741	m
DMMO VWR 7	23	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 24	24	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	15	-21.894792	m
DMMO VWR 7	24	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 25	25	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	16	-27.834843	m
DMMO VWR 7	25	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 26	26	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	17	-33.774894	m
DMMO VWR 7	26	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 27	27	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	18	-39.714945	m
DMMO VWR 7	27	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 28	28	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	19	-45.654996	m
DMMO VWR 7	28	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 29	29	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	20	-51.595047	m
DMMO VWR 7	29	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 30	30	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	21	-57.535098	m
DMMO VWR 7	30	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 31	31	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	22	-63.475149	m
DMMO VWR 7	31	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 32	32	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	23	-69.415200	m
DMMO VWR 7	32	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 33	33	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	24	-75.355251	m
DMMO VWR 7	33	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 34	34	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	25	-81.295302	m
DMMO VWR 7	34	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 35	35	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	26	-87.235353	m
DMMO VWR 7	35	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 36	36	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	27	-93.175404	m
DMMO VWR 7	36	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 37	37	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	28	-99.115455	m
DMMO VWR 7	37	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 38	38	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	29	-105.055506	m
DMMO VWR 7	38	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 39	39	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	30	-110.995557	m
DMMO VWR 7	39	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 40	40	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	31	-116.935608	m
DMMO VWR 7	40	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 41	41	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	32	-122.875659	m
DMMO VWR 7	41	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 42	42	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	33	-128.815710	m
DMMO VWR 7	42	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 43	43	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	34	-134.755761	m
DMMO VWR 7	43	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 44	44	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	35	-140.695812	m
DMMO VWR 7	44	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 45	45	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	36	-146.635863	m
DMMO VWR 7	45	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 46	46	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	37	-152.575914	m
DMMO VWR 7	46	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 47	47	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	38	-158.515965	m
DMMO VWR 7	47	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 48	48	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	39	-164.456016	m
DMMO VWR 7	48	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 49	49	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	40	-170.396067	m
DMMO VWR 7	49	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 50	50	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	41	-176.336118	m
DMMO VWR 7	50	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 51	51	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	42	-182.276169	m
DMMO VWR 7	51	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 52	52	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	43	-188.216220	m
DMMO VWR 7	52	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 53	53	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	44	-194.156271	m
DMMO VWR 7	53	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 54	54	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	45	-200.096322	m
DMMO VWR 7	54	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 55	55	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	46	-206.036373	m
DMMO VWR 7	55	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 56	56	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	47	-211.976424	m
DMMO VWR 7	56	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 57	57	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	48	-217.916475	m
DMMO VWR 7	57	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 58	58	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	49	-223.856526	m
DMMO VWR 7	58	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 59	59	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	50	-229.796577	m
DMMO VWR 7	59	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 60	60	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	51	-235.736628	m
DMMO VWR 7	60	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 61	61	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	52	-241.676679	m
DMMO VWR 7	61	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 62	62	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	53	-247.616730	m
DMMO VWR 7	62	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 63	63	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	54	-253.556781	m
DMMO VWR 7	63	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 64	64	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	55	-259.496832	m
DMMO VWR 7	64	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 65	65	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	56	-265.436883	m
DMMO VWR 7	65	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 66	66	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	57	-271.376934	m
DMMO VWR 7	66	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 67	67	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	58	-277.316985	m
DMMO VWR 7	67	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 68	68	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	59	-283.257036	m
DMMO VWR 7	68	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 69	69	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	60	-289.197087	m
DMMO VWR 7	69	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 70	70	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	61	-295.137138	m
DMMO VWR 7	70	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 71	71	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	62	-301.077189	m
DMMO VWR 7	71	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 72	72	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	63	-307.017240	m
DMMO VWR 7	72	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 73	73	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	64	-312.957291	m
DMMO VWR 7	73	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 74	74	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	65	-318.897342	m
DMMO VWR 7	74	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 75	75	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	66	-324.837393	m
DMMO VWR 7	75	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 76	76	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	67	-330.777444	m
DMMO VWR 7	76	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 77	77	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	68	-336.717495	m
DMMO VWR 7	77	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 78	78	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	69	-342.657546	m
DMMO VWR 7	78	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 79	79	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	70	-348.597597	m
DMMO VWR 7	79	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 80	80	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	71	-354.537648	m
DMMO VWR 7	80	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 81	81	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	72	-360.477699	m
DMMO VWR 7	81	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 82	82	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	73	-366.417750	m
DMMO VWR 7	82	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 83	83	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	74	-372.357801	m
DMMO VWR 7	83	0.2302 4	90 13 43.7978	0.13	WY	DMMO VWR 84	84	0.2302 4	80 17 91.492	0.13	DEPT GEA 17	75	-378.297852	m
DMMO VWR 7	84	0.2302 4	90 13											

Annex 3: SINEX file

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+FILE/COMMENT
* File created by software tosinex (J.López-Ramascó)*
* Matrix scaling Factor used 1.0000000
-FILE/COMMENT
+-----+
+SITE/ID
+CODE PT _DOMES_ T _STATION DESCRIPTION_ APPROX_LON_ APPROX_LAT_ APP_H_
YEB1 A 13420M002 13420M002 -3 5 24.7 40 31 25.6 975.4
7389 A 13420S003 13420S003 -3 5 18.7 40 31 24.5 977.1
7386 A 13420S002 13420S002 -3 5 12.7 40 31 28.8 987.7
YEBE A 13420M001 13420M001 -3 5 19.1 40 31 29.6 972.8
-SITE/ID
+-----+
+SOLUTION/EPOCHS
+Code PT SOLN T Data_start_ Data_end_ Mean_epoch_
-SOLUTION/EPOCHS
+-----+
+SOLUTION/ESTIMATE
+INDEX TYPE CODE PT SOLN REF_EPOCH UNIT S ESTIMATED VALUE STD_DEV
1 STAX YEB1 A 1 16:313:00000 m 2 0.484880012006000E+07 0.60000E-03
2 STAY YEB1 A 1 16:313:00000 m 2 -.261769158390000E+06 0.40000E-03
3 STAZ YEB1 A 1 16:313:00000 m 2 0.412300148813000E+07 0.50000E-03
4 STAX 7389 A 1 16:313:00000 m 2 0.484883106750900E+07 0.60000E-03
5 STAY 7389 A 1 16:313:00000 m 2 -.261629454480000E+06 0.40000E-03
6 STAZ 7389 A 1 16:313:00000 m 2 0.412297653236000E+07 0.50000E-03
7 STAX 7386 A 1 16:313:00000 m 2 0.484876177517000E+07 0.14000E-02
8 STAY 7386 A 1 16:313:00000 m 2 -.261484111180000E+06 0.12000E-02
9 STAZ 7386 A 1 16:313:00000 m 2 0.412308509127400E+07 0.18000E-02
10 STAX YEBE A 1 16:313:00000 m 2 0.484872459568000E+07 0.60000E-03
11 STAY YEBE A 1 16:313:00000 m 2 -.261631978730000E+06 0.40000E-03
12 STAZ YEBE A 1 16:313:00000 m 2 0.412309430430000E+07 0.50000E-03
-SOLUTION/ESTIMATE
+-----+
+SOLUTION/MATRIX_ESTIMATE L COVA
+PARA1 PARA2 PARA2+0 PARA2+1 PARA2+2
1 1 0.399349803703331E-06
2 1 -.949745450350327E-08 0.171168170090582E-06
3 1 0.417274350354161E-07 -.215689230528934E-07 0.305024243443326E-06
4 1 0.266887877232670E-06 0.874849816854087E-08 0.111828279764368E-06
4 4 0.352588594421265E-06
5 1 -.289275289064266E-07 0.898853392886134E-07 0.815333859514687E-09
5 4 -.343912345618522E-07 0.180212059664241E-06
6 1 0.106790441831226E-06 -.419993973828026E-07 0.154677227003315E-06
6 4 0.937010342333650E-07 0.988469098495230E-08 0.246837283639591E-06
7 1 0.232786619031969E-06 -.387992217881363E-07 0.136757568192243E-06
7 4 0.273575979860889E-06 -.574103490237298E-07 0.883326262985326E-07
7 7 0.198506463052522E-05
8 1 -.457573175913036E-07 0.629717610499311E-07 0.180065474574056E-07
8 4 -.220263602003546E-07 0.516251025170187E-07 -.10265375626262653E-07
8 7 -.858595548644221E-09 0.153879265490230E-05
9 1 0.142023651941708E-06 0.111923977407388E-07 0.116522002164866E-06
9 4 0.929094731006245E-07 0.337932727295365E-07 0.175798348891874E-06
9 7 0.464825752863313E-07 -.328514736743445E-07 0.328146191189655E-05
10 1 0.257017792179926E-06 -.297280680062906E-07 0.11207779211696E-06
10 4 0.271561991649125E-06 -.369267612678623E-07 0.935458769524691E-07
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10 10 0.319196156852729E-06
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12 7 0.845968459108923E-07 -.458397437212257E-07 0.194557187140205E-06
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-SOLUTION/MATRIX_ESTIMATE L COVA
$ENDSNX

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